

**EE16B, Spring 2018
UC Berkeley EECS**

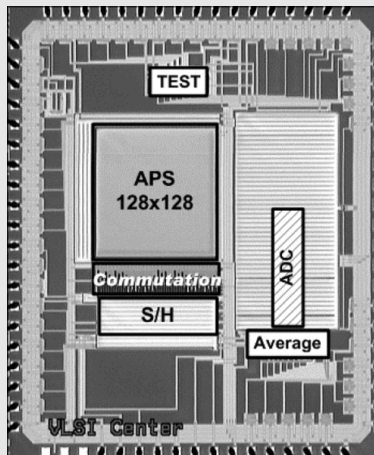
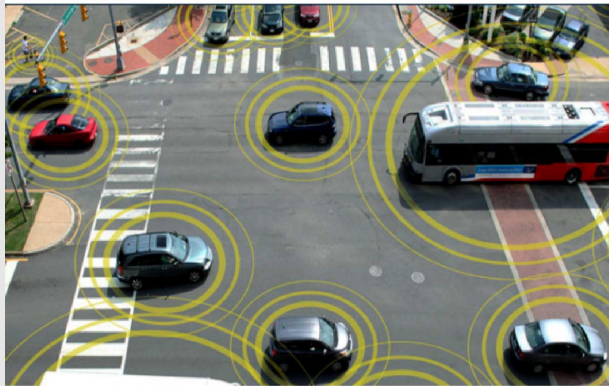
Maharbiz and Roychowdhury

Lecture 4A: Overview Slides

State Space Representations

Systems

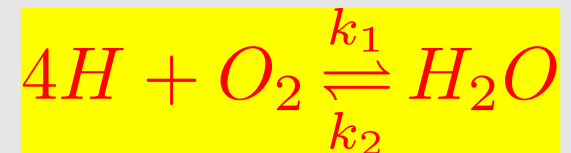
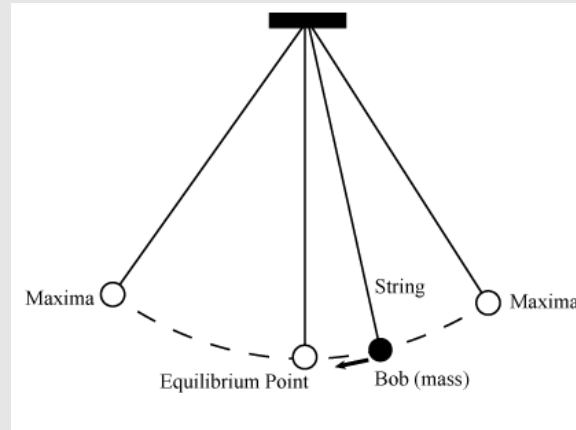
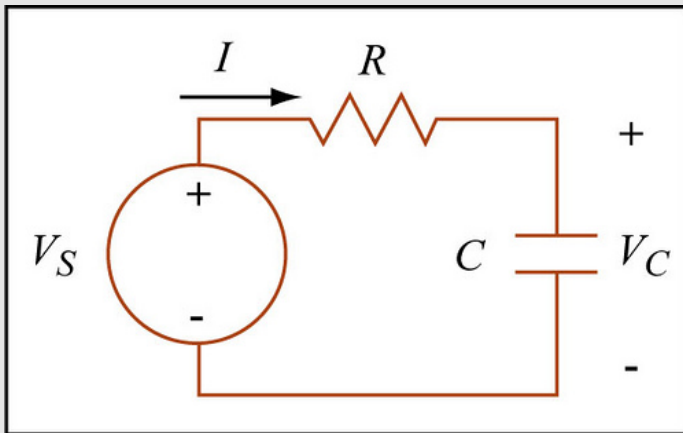
- Previously: circuits
- **Now: systems**
 - circuits + more: a broader concept



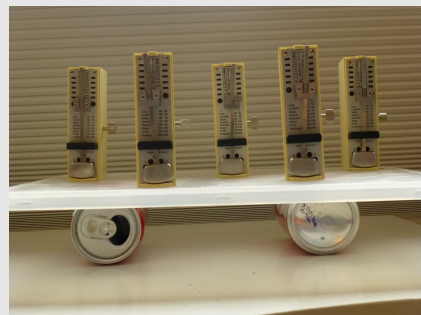
- **Can be enormously complex**
- **multi-domain**
 - EE (control, comm., computing, ...)
 - mech., chem., optical, ...
- **hierarchy of sub-systems**

Simpler Systems

- ... easier to understand and to work with

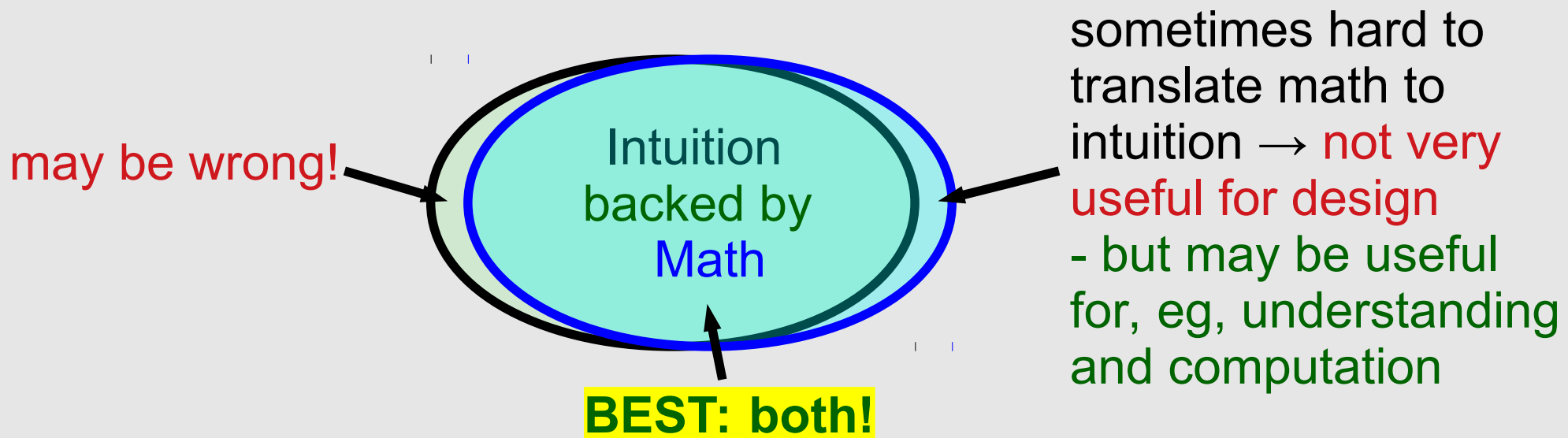


- Even small and simple systems can do interesting things



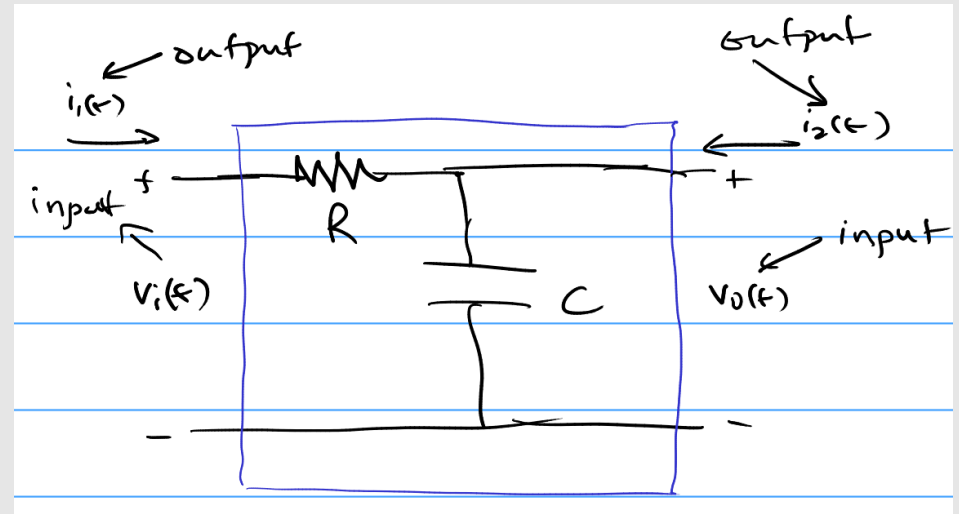
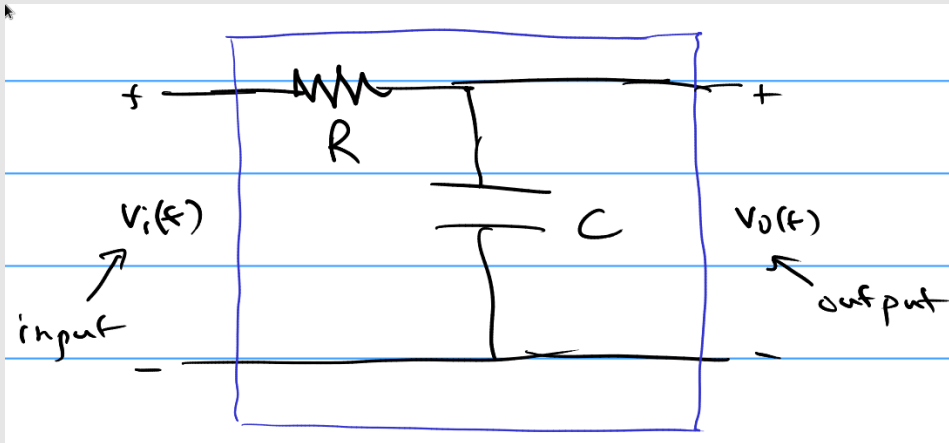
A Note about Intuition vs Math

- Proper intuition: extremely important
 - quickly make **mental leaps** to solve problems and design new things
 - ... **avoiding confusion** that can arise from masses of detail
- **Intuition doesn't arise magically**
 - mathematics: essential for **in-depth** understanding
 - math + experience and practice → intuition



Inputs and Outputs as **VECTORS**

- (move to xournal)



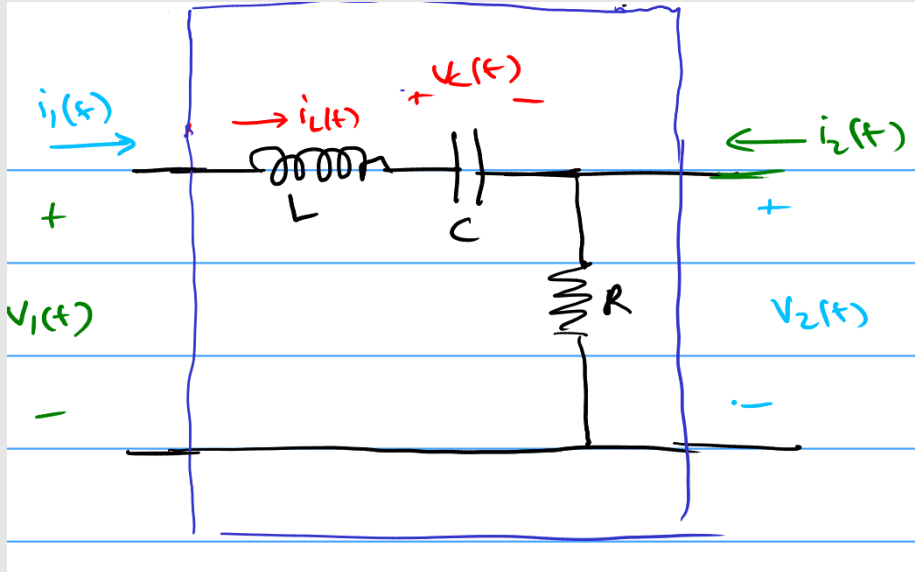
$$\vec{u}(t) = \begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix} ; \vec{y}(t) = \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

Annotations: "vector of inputs" points to $\vec{u}(t)$ and "vector of outputs" points to $\vec{y}(t)$. Both vectors are circled in red.

INPUTS AND OUTPUTS CAN BE ORGANIZED AS VECTORS

The Internal State

- (move to xournal)



$$\vec{w}(t) = \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix} \quad \vec{y}(t) = \begin{bmatrix} v_2(t) \\ i_1(t) \end{bmatrix}$$

$$\vec{x}(t) = \begin{bmatrix} v_c(t) \\ i_L(t) \end{bmatrix}$$

- Internal voltages/currents (unknowns): the **state**
 - also written as a vector: $\vec{x}(t)$

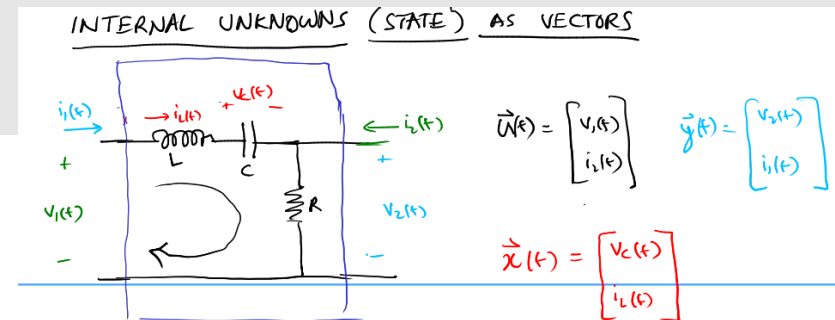
The System's Equations

- (move to xournal)

EQUATIONS

Capacitor + KCL : $C \frac{dv_c(t)}{dt} - i_L(t) = 0$

KVL : $L \frac{di_L(t)}{dt} + v_c(t) + R(i_L(t) + i_2(t)) - v_1(t) = 0$



$$\underbrace{\begin{bmatrix} C & 0 \\ 0 & L \end{bmatrix}}_A \frac{d}{dt} \underbrace{\begin{bmatrix} v_c(t) \\ i_L(t) \end{bmatrix}}_{\vec{x}(t)} + \underbrace{\begin{bmatrix} 0 & -1 \\ 1 & R \end{bmatrix}}_B \underbrace{\begin{bmatrix} v_c(t) \\ i_L(t) \end{bmatrix}}_{\vec{x}(t)} + \underbrace{\begin{bmatrix} 0 & 0 \\ -1 & R \end{bmatrix}}_C \underbrace{\begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}}_{\vec{u}(t)} = \underbrace{\begin{bmatrix} 0 \\ 0 \end{bmatrix}}_0$$

$$\frac{d}{dt} \begin{bmatrix} v_c(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} 0 & 1/C \\ -1/L & -R/L \end{bmatrix} \begin{bmatrix} v_c(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 1/L & -R/L \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

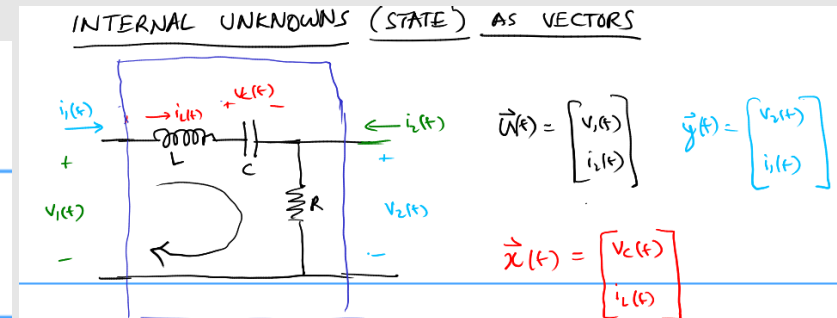
- can be written using the **input** and **state vectors**

The Outputs

- (move to xournal)

$$v_2(t) = R(i_L(t) + i_2(t))$$

$$i_1(t) = i_L(t)$$



$$\vec{y}(t) = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \vec{x}(t) + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_F \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

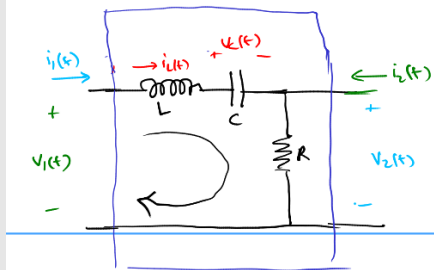
- also expressed using the **input** and **state vectors**

State+Output Eqns Together

$$\frac{d}{dt} \begin{bmatrix} v_L(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} 0 & 1/L \\ -1/L & -R/L \end{bmatrix} \begin{bmatrix} v_L(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} 1/L \\ 1/L \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

$\xleftarrow{\vec{f}(\vec{x}, \vec{u})}$
 $\xrightarrow{\vec{g}(\vec{x}, \vec{u})}$

INTERNAL UNKNOWN(S) (STATE) AS VECTORS



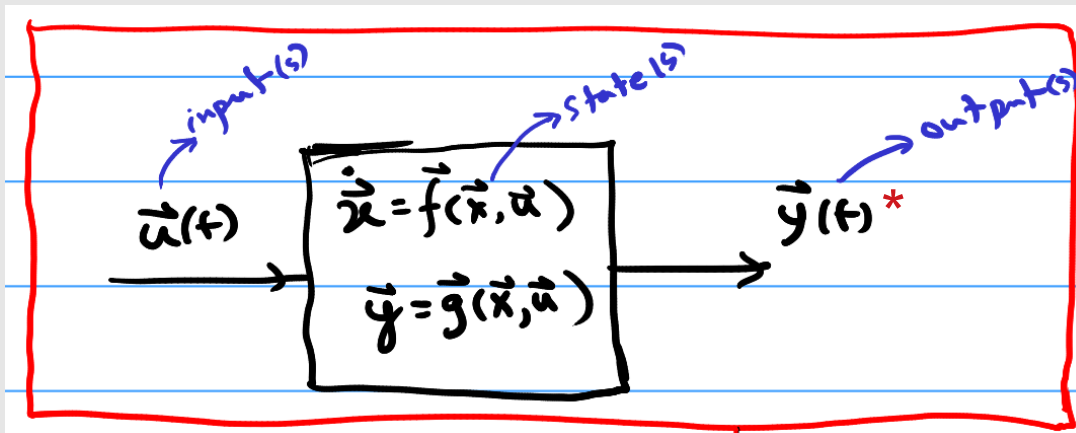
$$\vec{u}(t) = \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix} \quad \vec{y}(t) = \begin{bmatrix} v_2(t) \\ i_1(t) \end{bmatrix}$$

$$\vec{x}(t) = \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}$$

$$\vec{y}(t) = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \underbrace{\begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}}_{\vec{x}(t)} + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_E \underbrace{\begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}}_{\vec{u}(t)}$$

• **general form:** $\frac{d}{dt} \vec{x}(t) = \vec{f}(\vec{x}(t), \vec{u}(t))$, $\vec{y}(t) = \vec{g}(\vec{x}(t), \vec{u}(t))$ + initial condition (IC)

STATE SPACE FORMULATION

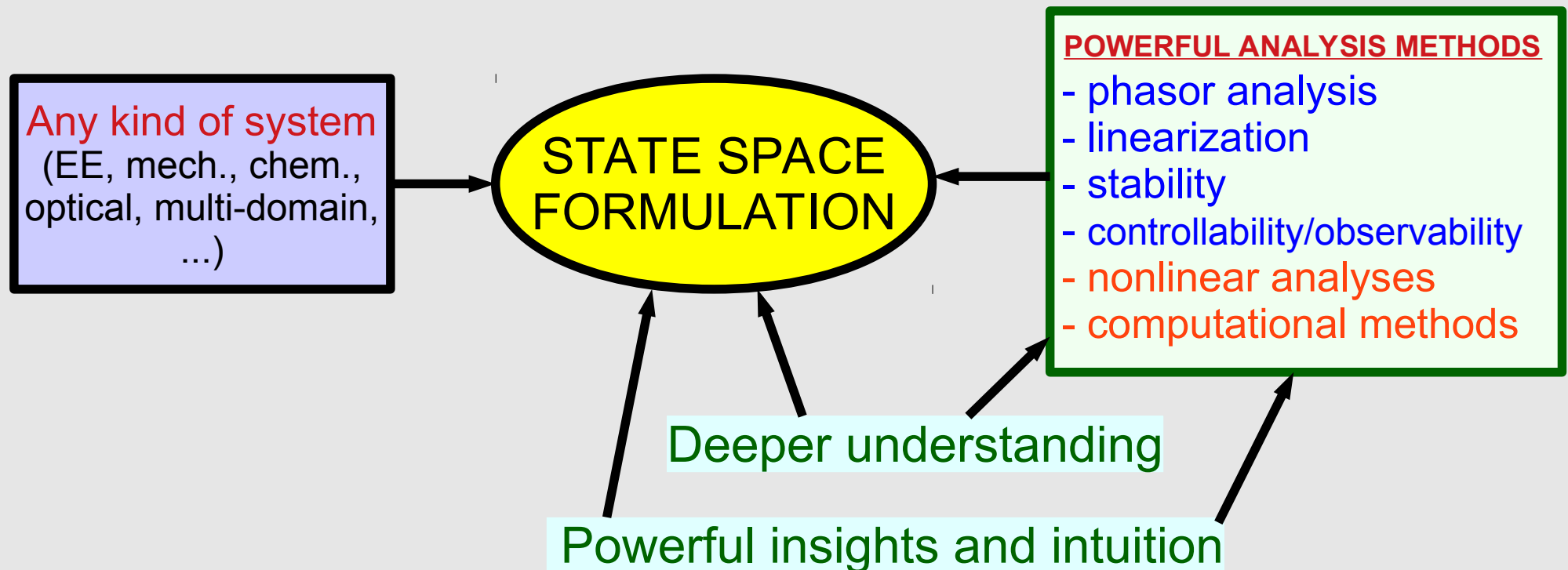


* if not explicitly given, the entire state will be the output.

State Space Formulation: Benefits

- why is it useful?

- any circuit can be written like this (not just this one)*
 - however big or complicated
- not just circuits – any system* from any domain!
 - including multi-domain systems



* some additional generalization needed – won't cover in this class

Previous Lecture

• examples

- RLC circuit
- pendulum

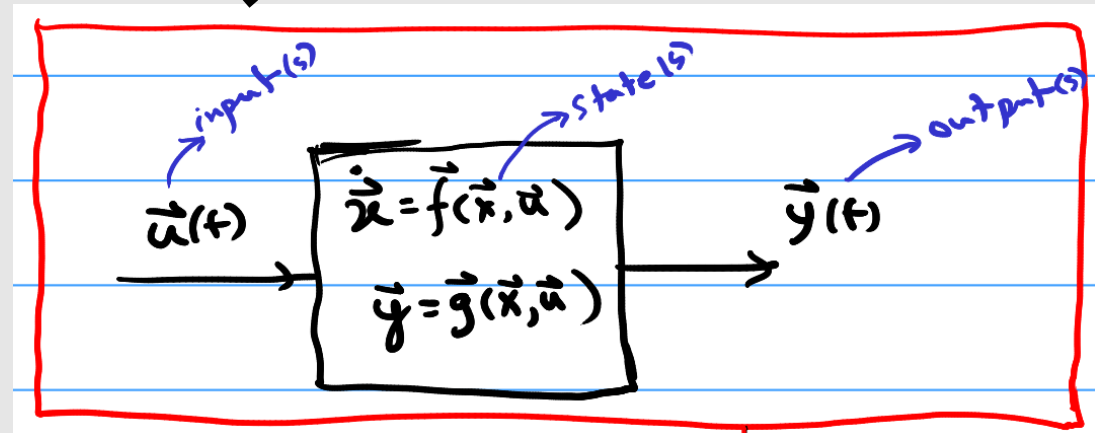
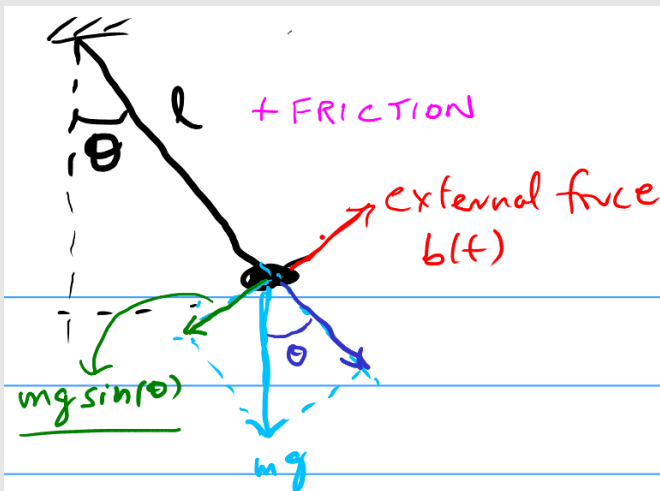
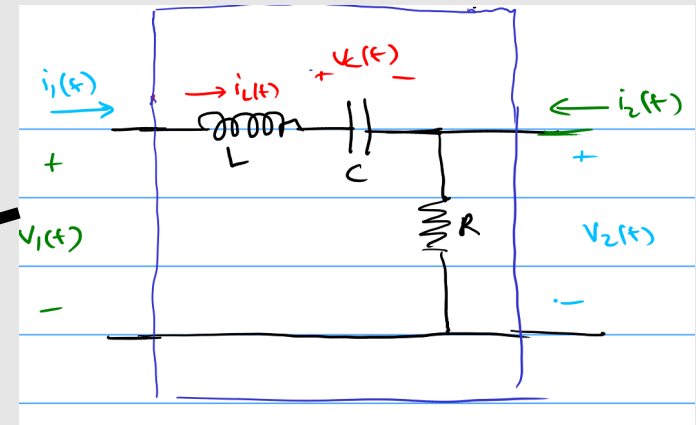
Any kind of system
(EE, mech., chem.,
optical, multi-domain,
...)

STATE SPACE FORMULATION

$$\frac{d}{dt}\vec{x}(t) = \vec{f}(\vec{x}(t), \vec{u}(t))$$

$$\vec{y}(t) = \vec{g}(\vec{x}(t), \vec{u}(t))$$

+ initial condition (IC)



Mechanical Example: Pendulum

- (move to xournal)

→ Newton's eqn. of motion: $\vec{F} = m\vec{a}$ or $\vec{a} = \frac{\vec{F}}{m}$

→ total tangential force =

force due to gravity : $-mg \sin(\theta)$

+ force " " friction : $-k \cdot \text{velocity}$

+ externally applied force : $b(t)$

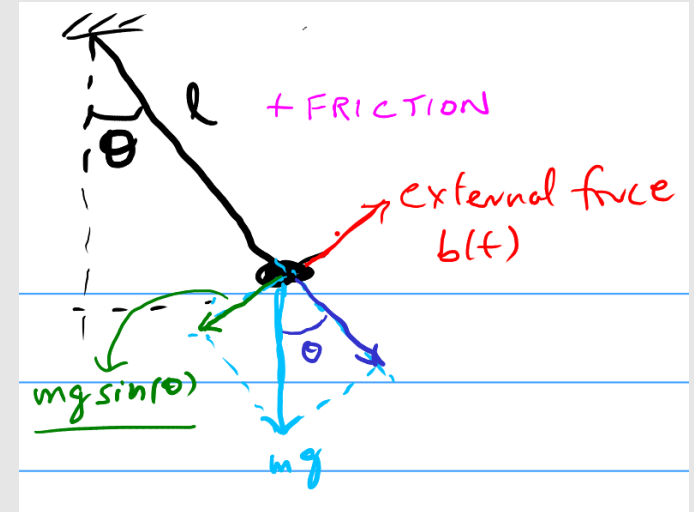
→ arc-length (from bottom) $\equiv y = l\theta$ θ in radians

→ velocity = $\frac{dy}{dt} = l \frac{d\theta}{dt}$
 $\underbrace{\quad}_{v_\theta}$

→ acceleration = $\frac{d^2 y}{dt^2} = l \frac{d^2 \theta}{dt^2} = l \frac{dv_\theta}{dt}$

→ total force : $-mg \sin(\theta) - k l \frac{d\theta}{dt} + b(t)$

→ $a = F/m \Rightarrow l \frac{d^2 \theta}{dt^2} = -g \sin(\theta) - \frac{k l}{m} \frac{d\theta}{dt} + \frac{b(t)}{m}$



$$\frac{d^2 \theta}{dt^2} = -\frac{g}{l} \sin(\theta) - \frac{k}{m} \frac{d\theta}{dt} + \frac{b(t)}{m l}$$

$$\vec{x} = \begin{bmatrix} \theta \\ v_\theta \end{bmatrix}, \quad \vec{u} = [b(t)]$$

$$\frac{d\vec{x}}{dt} = \begin{bmatrix} v_\theta \\ -\frac{g}{l} \sin(\theta) - \frac{k}{m} v_\theta + \frac{b(t)}{m l} \end{bmatrix}$$

- The system is nonlinear (because of $\sin(\dots)$)

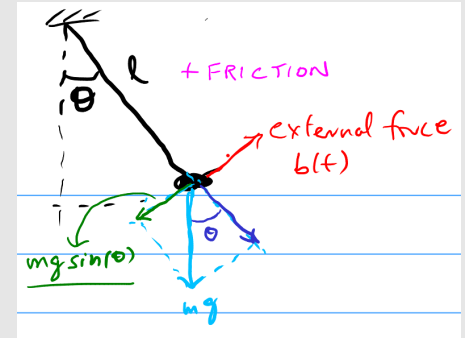
Pendulum: simplification for small θ

- $$\frac{d\vec{x}}{dt} = \begin{bmatrix} v_\theta \\ -g/l \sin(\theta) - k/m v_\theta + \frac{b(t)}{ml} \end{bmatrix}$$

– if θ is small (check in MATLAB)

→ $\sin(\theta) \approx \theta$ (in radians)

→ example of linearization



$$\frac{d\vec{x}}{dt} = \begin{bmatrix} 0 & 1 \\ -g/l & -\frac{k}{m} \end{bmatrix} \vec{x}(t) + \begin{bmatrix} 0 \\ \frac{1}{ml} \end{bmatrix} \vec{u}(t)$$

- Does this look familiar?

$$\frac{d}{dt} \begin{bmatrix} v_L(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} -\frac{1}{L} & \frac{1}{L} \\ \frac{1}{L} & -\frac{R}{L} \end{bmatrix} \begin{bmatrix} v_L(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} \frac{1}{L} \\ -\frac{R}{L} \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

- INSIGHT:** RLC ckt and damped pendulum are “the same”!

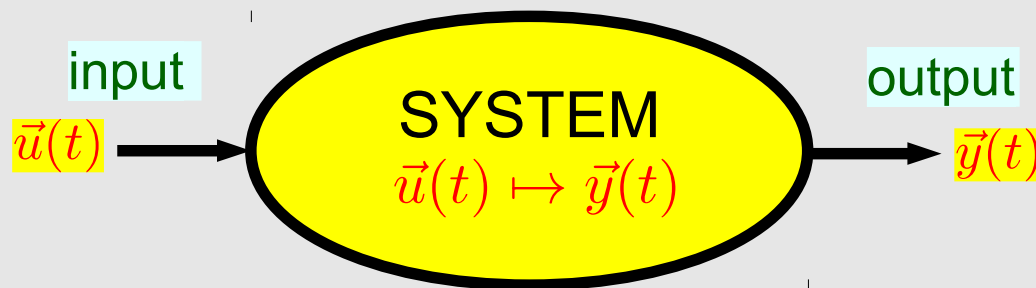
Filters

Filters??

MEMS filters!
(smaller, better, cheaper)

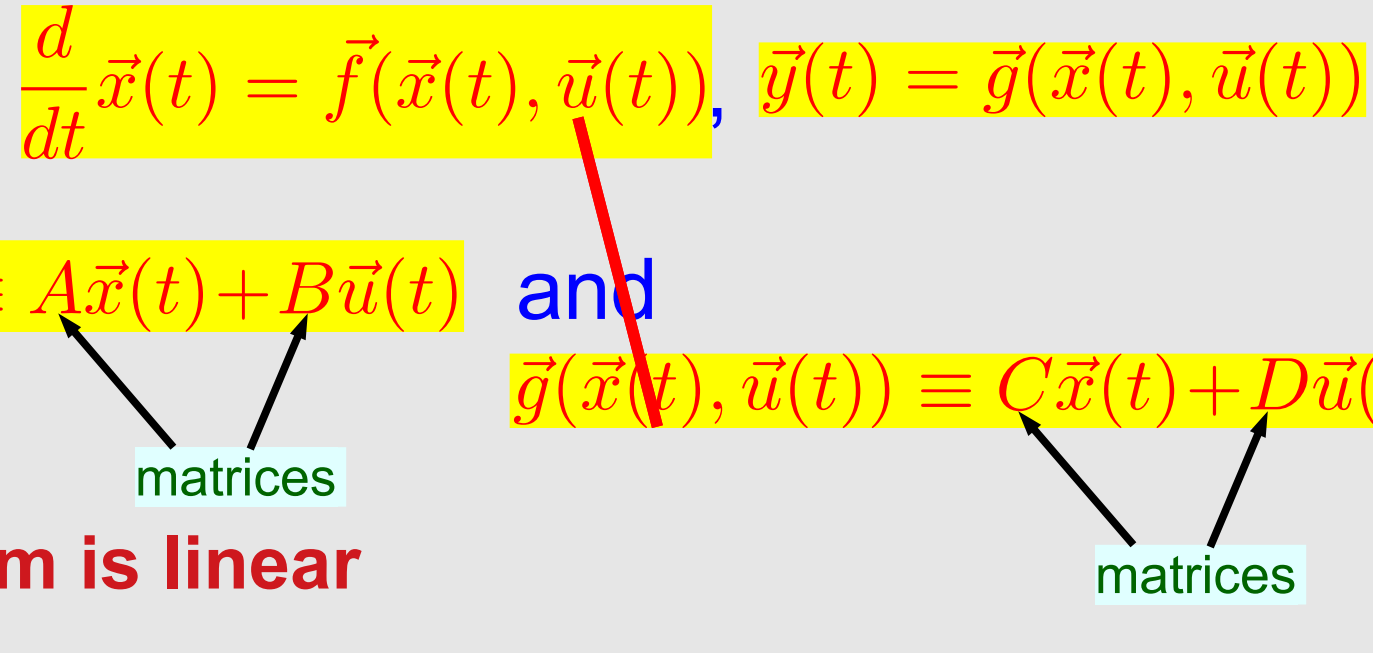
Recap of Linearity

- The concept of **LINEARITY** is extremely important
- **it is fundamentally a systems concept**

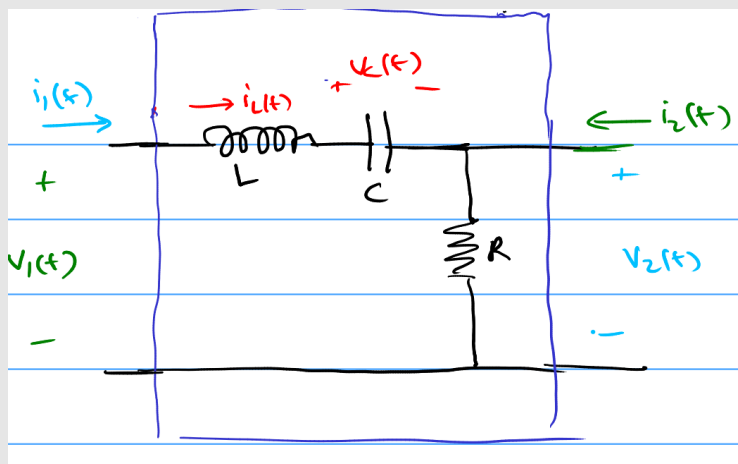


- 3 steps to check linearity
 - **clearly identify your inputs and outputs (this affects linearity)**
 - **check superposition**
 - if $\vec{u}_1(t) \mapsto \vec{y}_1(t)$ and $\vec{u}_2(t) \mapsto \vec{y}_2(t)$, then $(\vec{u}_1(t) + \vec{u}_2(t)) \mapsto (\vec{y}_1(t) + \vec{y}_2(t))$, $\forall \vec{u}_1(t), \vec{u}_2(t)$
 - **check scaling**
 - if $\vec{u}(t) \mapsto \vec{y}(t)$, then $(\alpha \vec{u}(t)) \mapsto (\alpha \vec{y}(t))$, $\forall \vec{u}(t)$ and $\forall \alpha \in \mathbb{R}$

Linearity of State Space Formulations

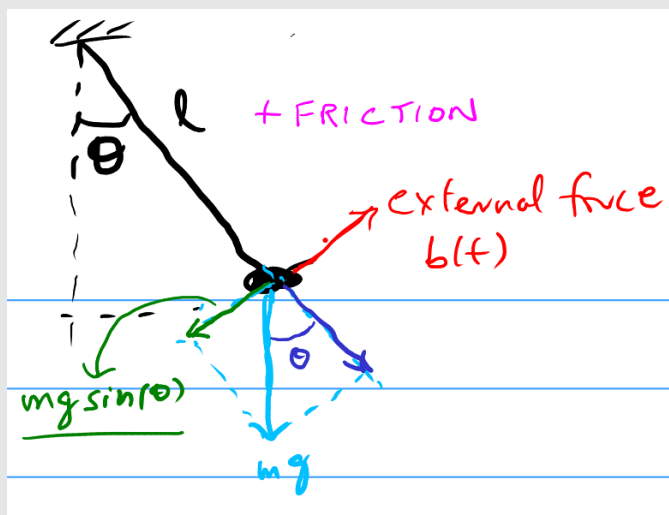
- general S.S.F: $\frac{d}{dt}\vec{x}(t) = \vec{f}(\vec{x}(t), \vec{u}(t)), \vec{y}(t) = \vec{g}(\vec{x}(t), \vec{u}(t))$
 - If $\vec{f}(\vec{x}(t), \vec{u}(t)) \equiv A\vec{x}(t) + B\vec{u}(t)$ and $\vec{g}(\vec{x}(t), \vec{u}(t)) \equiv C\vec{x}(t) + D\vec{u}(t)$
 - then the system is linear
 - Proof?
- 

Are these Systems Linear?



$$\frac{d}{dt} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} 0 & 1/C \\ -1/L & -R/L \end{bmatrix} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} 0 & 1/C \\ 1/L & -R/L \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

$$\begin{bmatrix} \dot{\vec{y}}(t) \\ \vec{y}(t) \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_E \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$



$$\vec{x} = \begin{bmatrix} \theta \\ v_\theta \end{bmatrix}, \quad \vec{u} = [b(t)]$$

$$\frac{d\vec{x}}{dt} = \begin{bmatrix} v_\theta \\ -g/l \sin(\theta) - k/m v_\theta + \frac{b(t)}{ml} \end{bmatrix}$$

$$\frac{d}{dt} \vec{x}(t) = \begin{bmatrix} v_\theta \\ -\frac{g}{l} \theta - \frac{k}{m} v_\theta + \frac{b(t)}{ml} \end{bmatrix}$$

State Space F. for Discrete Time Systems

- What is a discrete-time system?
 - example: compound interest
 - (move to xournal)

— Example: compound interest
 — Principal P
 — Annual rate of interest r , compounded monthly. DISCRETE (integer, not real number)
 — Savings $S[t] = S[t-1] + \frac{r}{12} S[t-1]$ → 1, 2, 3, ...
 with $S[0] = P$ INITIAL CONDITION
 — Additions/withdrawals each month: $u[t]$
 — $S[t] = S[t-1] + \frac{r}{12} S[t-1] + u[t]$ → 1, 2, 3
 with $S[0] = P$
 DISCRETE TIME

- general form: $\vec{x}[t+1] = \vec{f}(\vec{x}[t], \vec{u}[t]), \vec{y}[t] = \vec{g}(\vec{x}[t], \vec{u}[t])$
 $t = 1, 2, 3, \dots$ + initial condition (IC) $\vec{x}[0]$ given

↑
STATE SPACE FORMULATION

- Discrete time sometimes more natural (eg, for finance, social dynamics, ...)

Another D.T. Example: Profs. and PhDs.

- (move to xournal)

- $p[t]$: no. of profs. in the US, year t ($t=1, 2, 3, \dots$)
- $r[t]$: no. of PhDs in year t
- γ : fraction of PhDs who become professors
- δ : fraction in each profession retiring
- $u[t]$: average number of PhD students graduated per prof. per year
 \uparrow can be manipulated by the professor (controlled by, eg, funding)
- Q: how do $p[t]$ and $r[t]$ evolve with time?

$$p[t+1] = p[t] - \delta p[t] + \gamma r[t]$$

$$r[t+1] = r[t] - \delta r[t] - \gamma r[t] + p[t] u[t]$$

— State space repr.?

$$\vec{x}[t] \triangleq \begin{bmatrix} p[t] \\ r[t] \end{bmatrix}; \quad \vec{f}(\vec{x}) = \begin{bmatrix} p(1-\delta) + \gamma r \\ r(1-\delta-\gamma) + pu \end{bmatrix}$$

- Linear?

VECTOR D.T. STATE-SPACE FORMULATION